

REPORT ON
SOIL INVESTIGATION FOR CONSTRUCTION OF
DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT
HEADQUARTER, ARWAL

Submitted to

CHIEF ENGINEER
BSEIDC, PATNA.

SHAMVWI CONSULTANT
414, Jagat Trade Centre,
Fraser Road, Patna – 800 001
Tel.: 0612 – 2973107, 2366308, 2365145
Fax: 0612 – 2214287
Mobile: +919835218184, 8986215718.

PREFACE

The present report on sub-soil investigation was carried out as per letter no BSEIDC/TECH/1960-5773 Dated 04.10.2019.

The entire investigation process was broadly divided into two category –one field work and second was laboratory work.

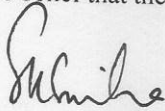
Field work includes conducting SPT ,Dynamic cone test, collection of disturbed as well as undisturbed soil samples from different location and different depth of sub-soil strata.

It was tried to get information from local people to get an idea about variation of water table during different season of year and also to get first hand information about type of foundation usually provided in the locality.

We thanks Prof. M.P.Jakhanwal ,M.Tech ,Ph.D. ,Muzaffarpur Institute of Technology, Muzaffarpur for his valuable advice during laboratory test and during preparation of report.

Client's help is gratefully acknowledged in providing Bore hole locations, cooperation and guidance during finalization of report.

We belief that the present report will serve the purpose, for which sub-soil investigation has been carried out.



Subodh Kumar Sinha

Partner, Shamvwi Consultant

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REPORT ON SUB-SOIL INVESTIGATION FOR THE CONSTRUCTION OF DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL.

1. INTRODUCTION

The objective of subsoil investigation reported here in, were taken up, to find out the nature of subsoil at the site of the proposed construction and to recommend the type or types of foundation suitable for it and the corresponding allowable bearing capacity.

The necessary field tests were carried out at the site. Soil samples from various depths in the different bore holes were collected, transported, carefully to the laboratory and tested to determine the engineering properties of the soil.

Based on the test results, certain recommendation were made and given in this report, regarding the type of foundation suitable for the proposed project and the allowable bearing capacity for certain sizes thereof.

2. TOPOGRAPHY

The land in question was even.

3. FIELD WORK

The field work consists of boring, soil sampling and conduct of Standard penetration tests and Dynamic cone penetration tests.

3.1 BORING

An appropriate number of boreholes of adequate depth were sunk at suitable spots as per direction of Engineer-in-charge. The details of the boreholes are given in table-1.

Table 1: Details of bore holes

DIAMETER OF BORE MM	DEPTH M	BORE HOLE
150	10.5	3 Bore Holes (BH-1 to BH-3)

The borings were kept dry while advancing through partially saturated soil. The position of water table in a borehole was recorded at least 48 hours after the stopping of the boring operation.

For boring below ground water level, the borehole was kept filled with water upto that level during boring.

3.2 SAMPLING

Undisturbed & disturbed samples were collected at different depth/where change of strata occurred. Identification slips were provided both inside and outside the tube.

On arrival in laboratory, the identification slips were checked against the boring and sampling records. Samples were extracted from the tubes just before testing.

3.3 STANDARD PENETRATION TEST

This test was performed in the boreholes at interval of depth of 1.5m, or at the change of starta/ as per IS: 2131 of 1963.

3.4 DYNAMIC CONE PENETRATION TEST

This test was performed when a bore hole could not be advanced to desired depth due to caving- in of the soil, or when it was felt necessary to supplement the information gained from SPT. This test was performed, as per

C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL

relevant IS code till high value of penetration resistance was encountered or till desired depth of investigation was reached, at which stage the test was stopped.

4. LABORATORY TEST

Lab. Test was performed to determine the following properties of soil samples as per relevant I.S. code.

- (a) Natural moisture content.
- (b) Bulk density.
- (c) Atterberg's limits (on fine grained soil only)
- (d) Grain size analysis.
- (e) Specific gravity.
- (f) Shear test.
- (i) Unconfined/triaxial compression tests for fine-grained soils.
- (ii) Direct shear test for coarse-grained soils.
- (g) Consolidation tests for fine grained soils.
- (h) Organic content, chemical test etc.
- (i) pH of soil and water.
- (j) Free swell Index
- (k) Crushing strength test (uniaxial)

4.1 SAMPLE EXTRACTION & PREPARATION OF TEST SPECIMENS

Samples for different tests were prepared as per method described in relevant IS code/as per method described in standard book.

4.2 ROUTINE CLASSIFICATION TESTS.

Tests for the determination of natural moisture content, bulk density, Atterberg's limit, grain size distribution and specific gravity were performed as per IS code on representative disturbed soil samples, wherever felt necessary. The results were used in classifying the soils of different strata as per IS code 1498-1970.

5.0 PRESENTATION OF TEST RESULT

Results were presented in table form on the following pages.

6.0 METHOD FOR CALCULATION OF ALLOWABLE BEARING CAPACITY

6.1 COHESIVE SOIL

Net ultimate bearing capacity was calculated as per IS-6403-1981.

$$q_d = cN_c S_c D_c I_c$$

q_d = net ultimate bearing capacity

$$N_c = 5.14$$

$S_c = 1$ for strip footing

$$D_c = 1 + 0.2 * D/B$$

$I_c = 1$ for vertical loading

c = cohesion obtained through unconfined compression test for depth of $2B/3$ below the foundation.

C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL

Settlement criteria

$$S = H / (1 + e_0) * C_c * \log((p_0 + p_1) / p_0)$$

S = settlement

H = thickness of compressible layer

e_0 = initial void ratio

p_0 = initial effective pressure

p_1 = pressure increment

C_c = compression index

6.2 Soil with the value of c & θ

Net ultimate bearing capacity was calculated as per IS 6403-1981

$$Q_d = c N_c S_c D_c I_c + q (N_q - 1) S_q D_q I_q + 0.5 R * B N_r * S_r * D_r * I_r * w'$$

For local shear failure

$$\tan \theta' = 0.67 * \tan \theta$$

$$C' = 2 * c / 3$$

$S_c = S_q = S_r = 1$ for strip footing

$$D_c = 1 + 0.2 * (D/B) * \tan(45 + \theta/2)$$

$I_c = I_q = I_r = 1$ for vertical loading

$$D_q = D_r = 1 + 0.1 * (D/B) \tan(45 + \theta/2)$$

$$q = (R - R_w) * D$$

M = moisture content

R = bulk density of soil

R_w = unit weight of water

L.L. = liquid limit

P.L. = plastic limit

S.L. = shrinkage limit

D = depth below ground level

Settlement criteria

The net allowable bearing capacity for a permissible settlement of 25mm, was obtained by

C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL

teng's formula

$$Q_{na} = 3.5 \cdot (N-3) \cdot \left\{ \frac{B+0.3}{2} \cdot B \right\} \cdot \left\{ \frac{B+0.3}{2} \cdot B \right\} \cdot w \cdot F_d$$

N = corrected N

$$F_d = 1 + D/B \quad \text{less than or equal to } 2$$

7.0 METHOD FOR CALCULATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part I/Sec 2-1979

7.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

$$Q = A_p \cdot N_c \cdot C_p + a \cdot C \cdot A_s$$

A_p = cross sectional area of pile toe in cm^2

N_c = Bearing capacity factor usually taken as 9

C_p = average cohesion at pile tip in Kg/cm

a = reduction factor

C = average cohesion throughout the length of pile in kg/cm^2

A_s = surface area of pile shaft in cm^2

8.0 METHOD FOR CALCULATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part III-1980

8.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

$$Q = A_p \cdot N_c \cdot C_p + A_a \cdot N_c \cdot C'_a + C'_a \cdot A_s' + \alpha \cdot C_a \cdot A_s$$

A_p = cross sectional area of pile toe in cm^2

N_c = Bearing capacity factor usually taken as 9

C_p = cohesion of soil around toe.

α = reduction factor

$$A_a = \pi \cdot (D_u^2 - D^2) / 4$$

C'_a = average cohesion around under ream

D_u = dia of under-ream, D = dia of pile

A_s' = surface area of pile shaft in cm^2

A_s = surface area of stem

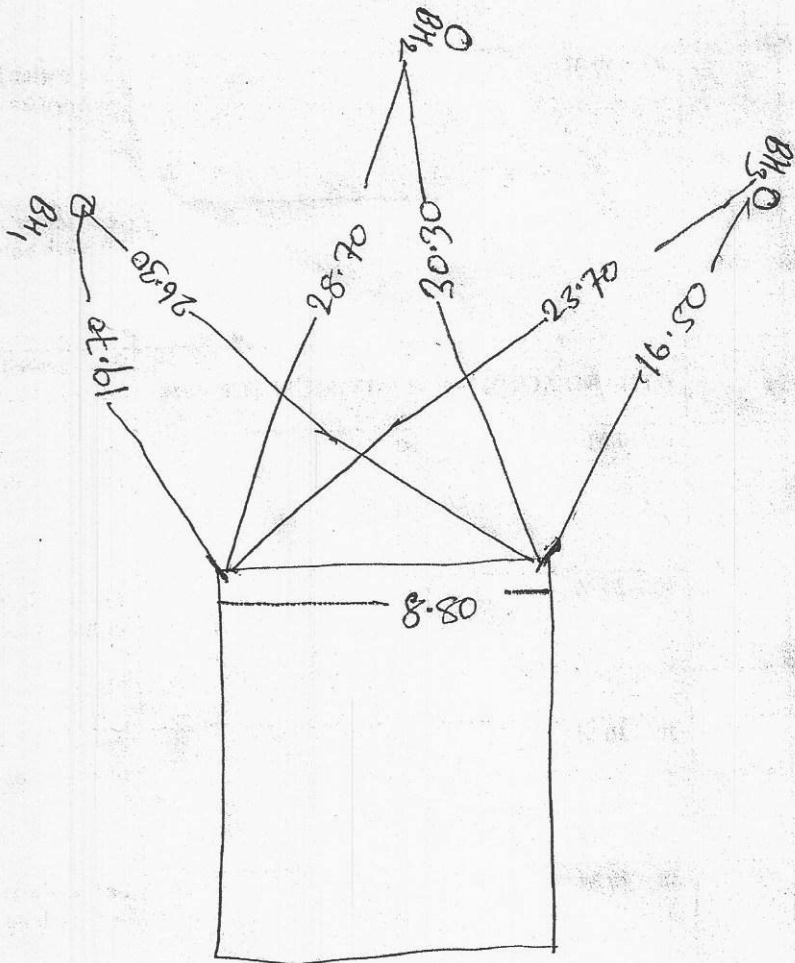
$A's$ = surface area of the cylinder circumscribing the under ream.



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कपुरस्थान

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परिमाण

Arwal to Goh Road

परिमाण

Neeraj Kumar
J.E (BSE/DG)
(Muzaffarpur Div)

SHAMWVI CONSULTANTS, 414J T.C., FRASE R ROAD, PATNA

SOIL TEST FOR C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL

TABLE NO. : 2

TERMINATION DEPTH : 10.5

BORE HOLE NO : BH1

START DATE : 16.11.2019

WATER TABLE DEPTH : 1.7M

FINISH DATE : 16.11.2019

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM	STANDARD PENETRATION RESISTANCE CURVE			GRAIN SIZE ANALYSIS	ATTERBERG'S LIMITS			DENSITY		SHEAR TEST			UNCONFINED COMPRESSION TEST, q	COEFFICIENT OF VOLUME COMPRESSION, m_v	
			OBSERVED VALUE	CORRECTED VALUE	5		10	20	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	TYPE OF TEST			COHESION c (kg/cm ²)
DS	G.L																
UDS 1																	
SPT1	1.5	13				GRAVEL (%) SAND (%) SILT (%) CLAY (%)	41	20	21	1.99	1.69	17.8	2.60	UUT	0.26	18.0	
UDS 2																	
SPT2	3	11				GRAVEL (%) SAND (%) SILT (%) CLAY (%)	32	26	6	1.96	1.71	14.5	2.62	UUT	0.16	29.00	
DS3																	
SPT3	4.5	10				GRAVEL (%) SAND (%) SILT (%) CLAY (%)	32	26	6	1.96	1.71	14.3	2.62	UUT	0.16	29.00	
UDS 4																	
SPT4	6	12				GRAVEL (%) SAND (%) SILT (%) CLAY (%)	35	20	15	2.00	1.62	23.6	2.61	UUT	0.3	23.00	

UCT : UNCONFINED COMPRESSION SHEAR TEST DST : DIRECT SHEAR TEST

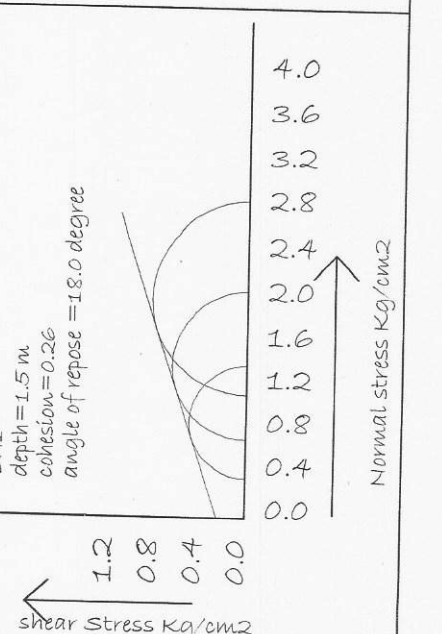
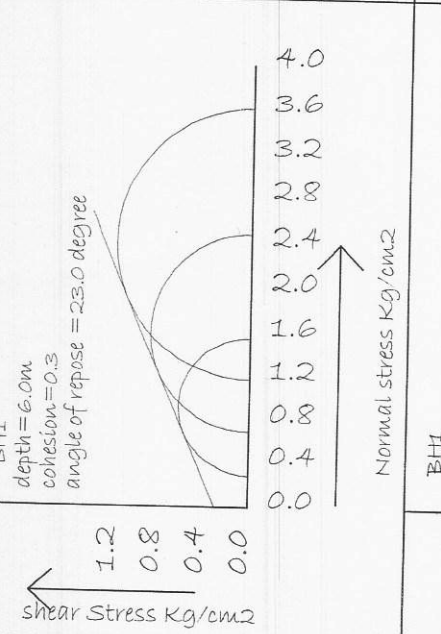
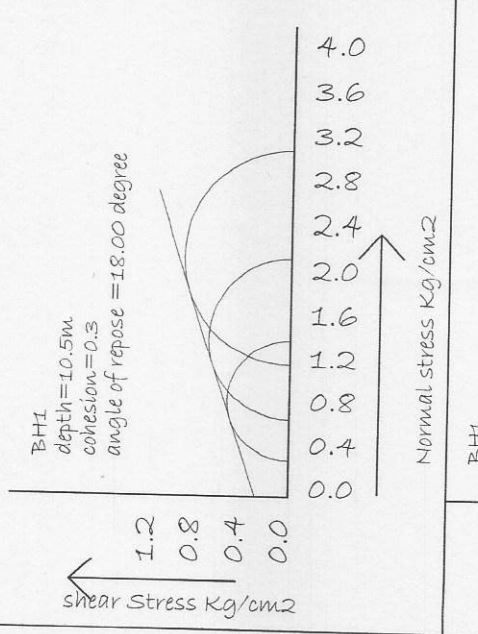
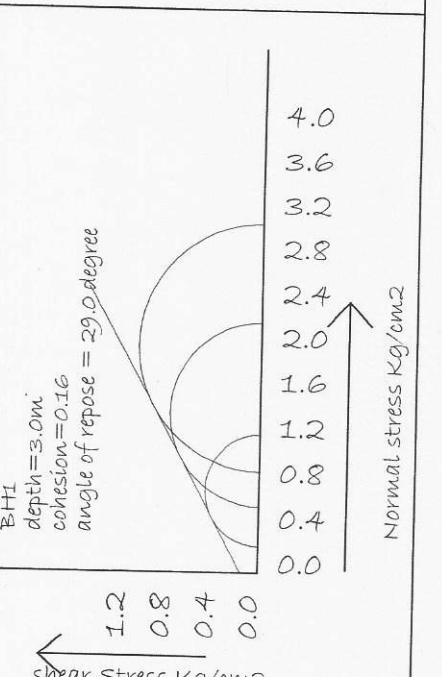
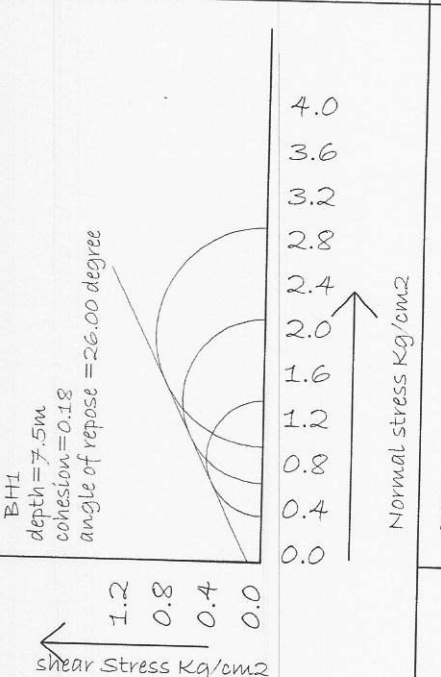
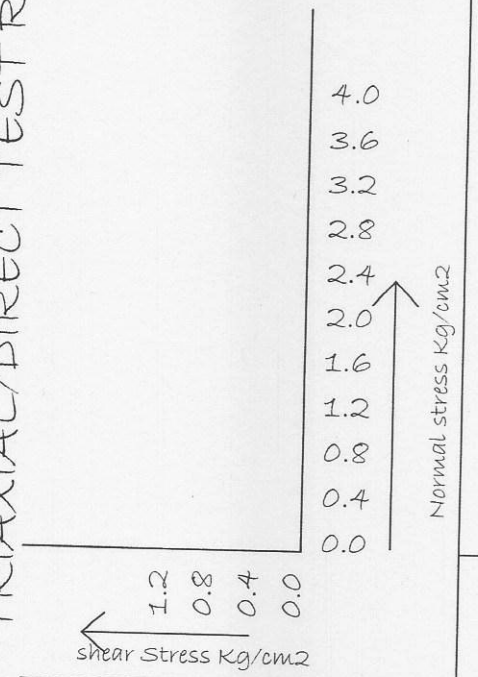
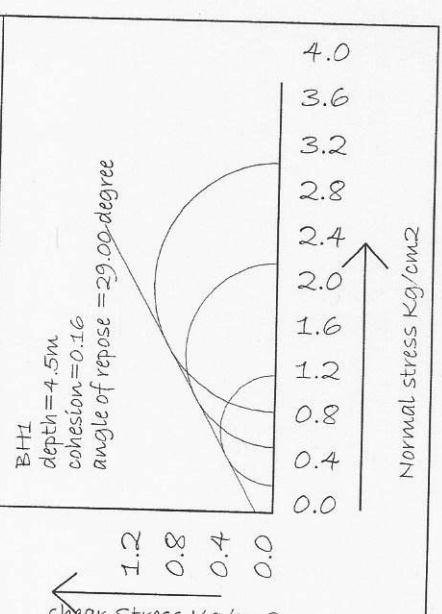
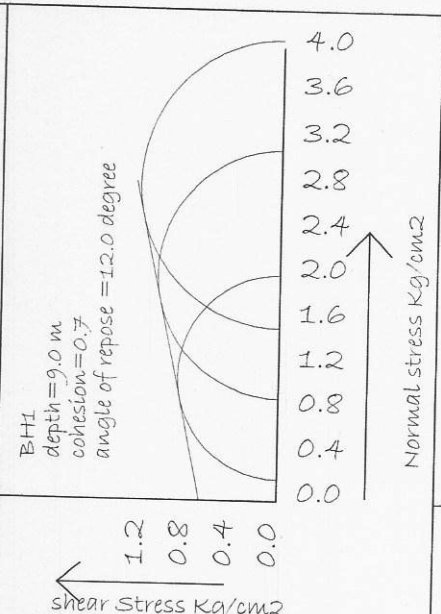
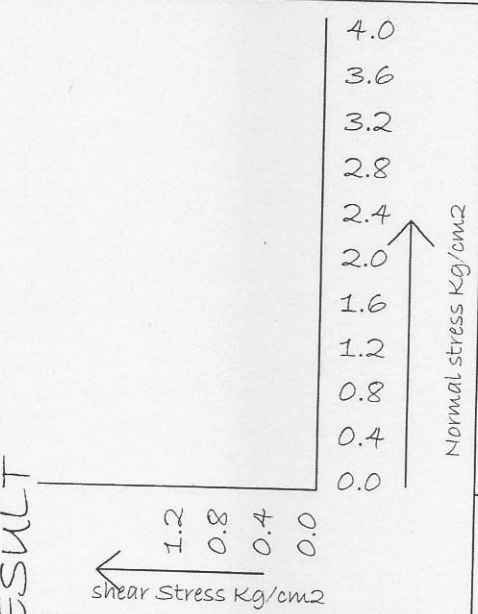
UDS : UNDISTURBED SAMPLE SPT : STANDARD PENETRATION TEST VALUE

NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m²

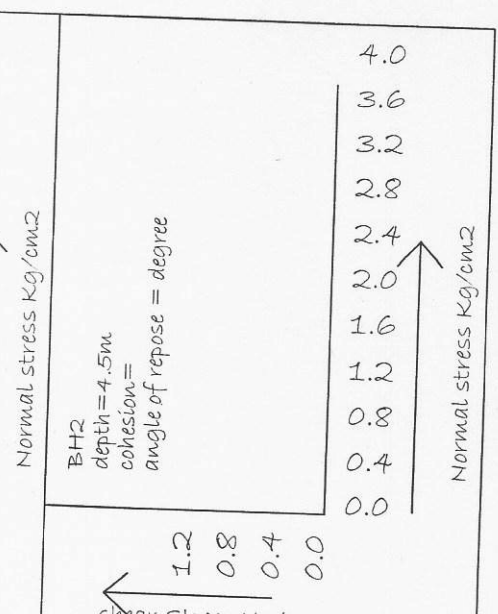
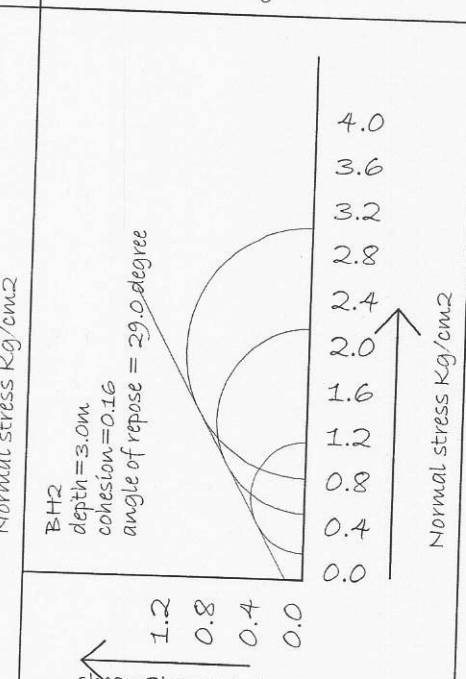
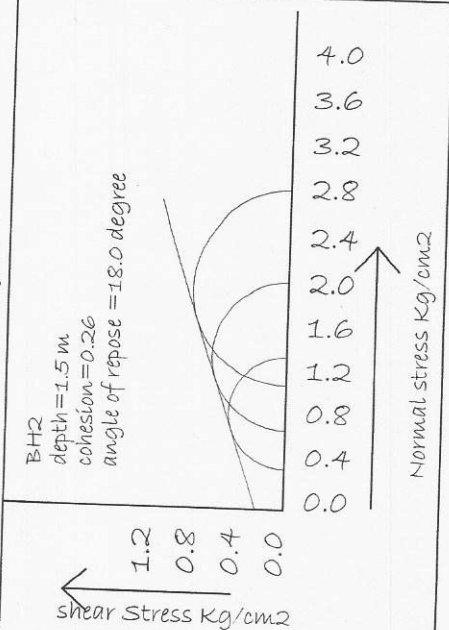
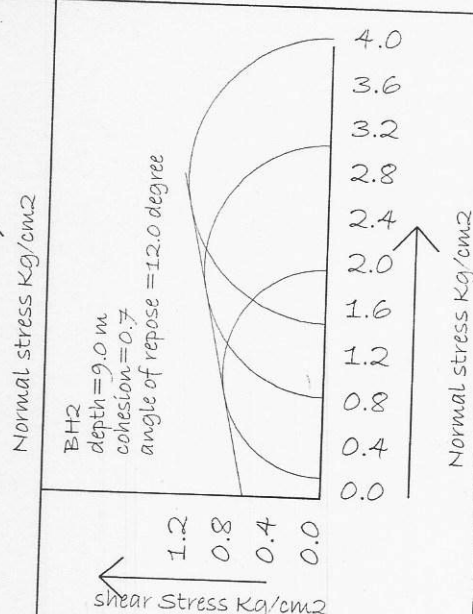
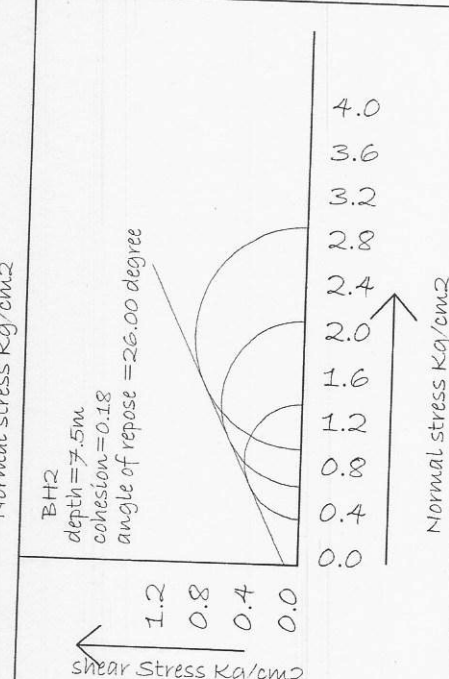
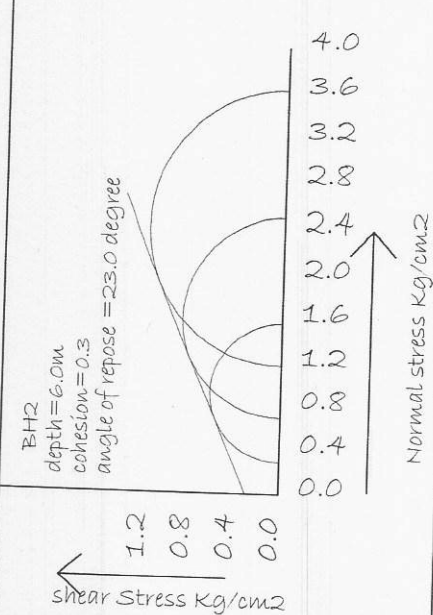
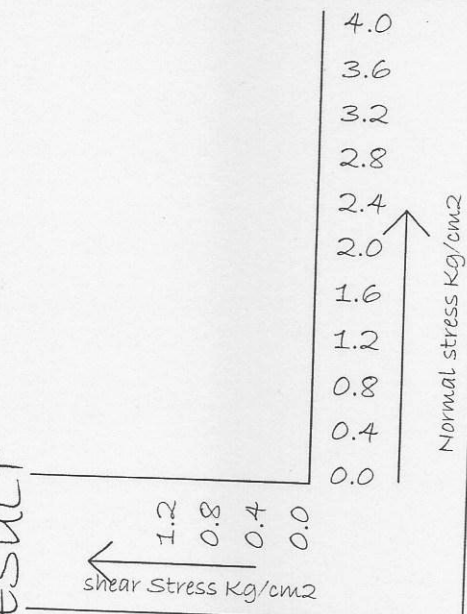
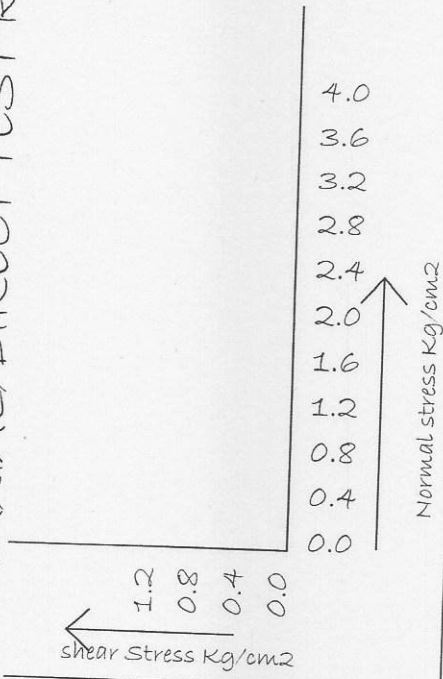
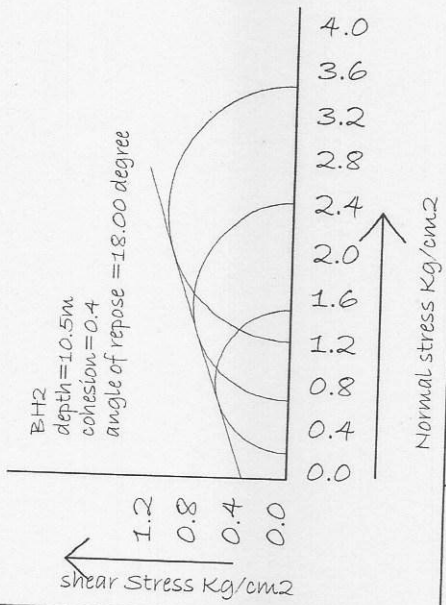
SHAMVVI CONSULTANTS 414J T. C. FRASE R ROAD, PATNA		SOIL TEST FOR C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL										TABLE NO. 5																								
SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY			NATURAL MOISTURE CONTENT (%)			SPECIFIC GRAVITY			SHEAR TEST			BORING DATES			TERMINATION DEPTH		WATER TABLE DEPTH		BORE HOLE NO		
		OBSERVED VALUE	CORRECTED VALUE	5	10	20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	NATURAL MOISTURE CONTENT (%)	GRAVITY	TYPE OF TEST	COHESION c (kg/cm ²)	ANGLE OF FRICTION IN DEGREE	VOID RATIO e ₀	COMPRESSION INDEX C _c	UNCONFINED COMPRESSION TEST q _u (kg/cm ²)	COEFFICIENT OF VOLUME COMPRESSIONITY M _v (cm ³ /kg)	START : 16.11.2019	FINISH : 17.11.2019	DEPTH : 10.5	DEPTH : 1.7M	: BH2						
UDS 5							Gravelly Sandy Silty Loam SC	18.3	43.20	38.5		35	18	17	1.97	1.62	21.6	2.62	UUT	0.18																
SPT5 7.5 24							Sandy Silty Clay CL	0.5	18.40	81.1		35	18	17	1.99	1.62	22.7	2.62	UUT	0.7	12.00															
UDS 6							Sandy Silty Clay CL	1.6	32.90	65.5		35	18	17	1.98	1.63	21.6	2.62	UUT	0.4	18.00															
SPT6 9.0 27																																				
UDS 7																																				
SPT7 10.5 30																																				
UUT - UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST		UCT : UNCONFINED COMPRESSION SHEAR TEST										DST : DIRECT SHEAR TEST																								
- SAMPLE SLIPED ~ TEST ON REMOULDED SAMPLE		UDS : UNDISTURBED SAMPLE																																		
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																																				
SPT : STANDARD PENETRATION TEST VALUE																																				

SHAMVVI CONSULTANTS 414J.T.C., FRASE R ROAD, PATNA		SOIL TEST FOR C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL												TABLE NO.: 7																
SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE			VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY			NATURAL MOISTURE CONTENT (%)			SPECIFIC GRAVITY			TYPE OF TEST	SHEAR TEST			UNCONFINED COMPRESSION TEST, q _u (kg/cm ²)	COEFFICIENT OF VOLUME COMPRESSION, m _v (cm ³ /kg)	
		OBSERVED VALUE	CORRECTED VALUE	5	10	20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm ³)	DRY DENSITY (gm/cm ³)	NATURAL MOISTURE CONTENT (%)	VOID RATIO, e _o	COMPRESSION INDEX, C _c	ANGLE OF FRICTION IN DEGREE	COHESION, c (kg/cm ²)									
UDS 5							Gravelly Sandy Silty Loam SC	17.8	44.50	37.7		35	18	17	1.97	1.59	23.6	2.62												
SPT5 7.5	22						Sandy Silty Clay CL	0.7	17.90	81.4		35	18	17	1.99	1.61	23.4	2.62												
UDS 6																														
SPT6 9.0	30																													
UDS 7																														
SPT7 10.5	30						Sandy Silty Clay CL	2.2	31.50	66.3		35	18	17	1.98	1.62	22.2	2.62												
UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST																			UCT : UNCONFINED COMPRESSION SHEAR TEST			DST : DIRECT SHEAR TEST								
! SAMPLE SLIPPED ~ TEST ON REMOULDED SAMPLE																			UDS : UNDISTURBED SAMPLE			SPT : STANDARD PENETRATION TEST VALUE								
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m ²																														

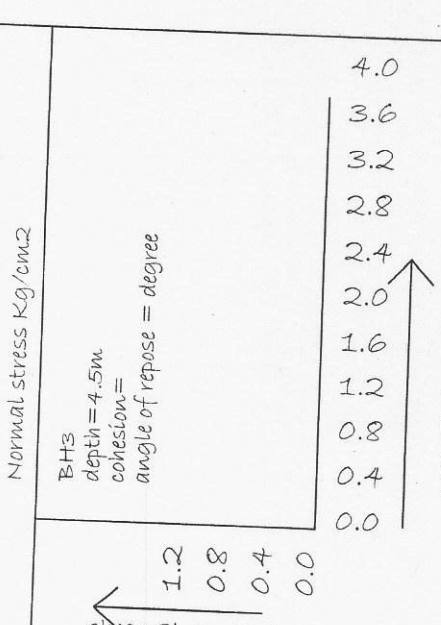
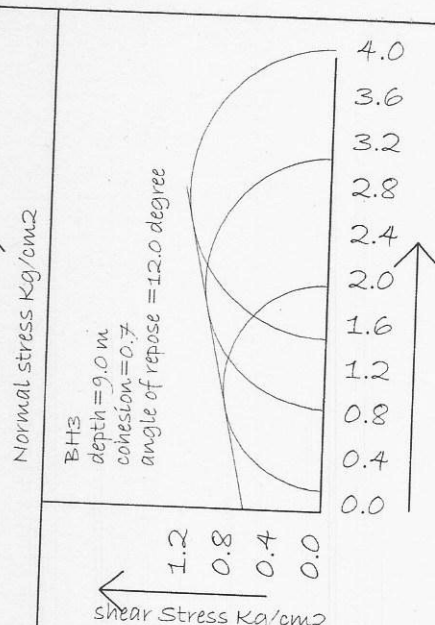
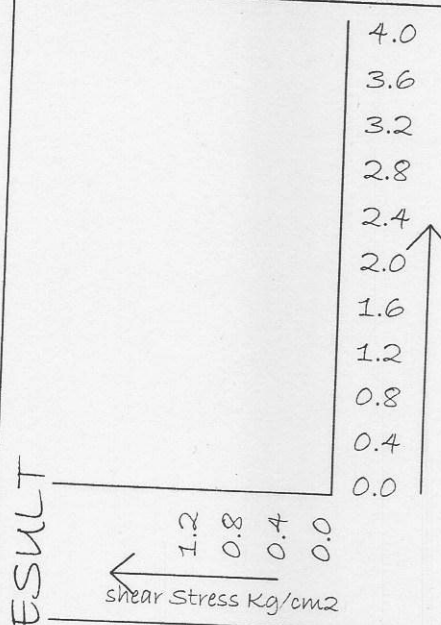
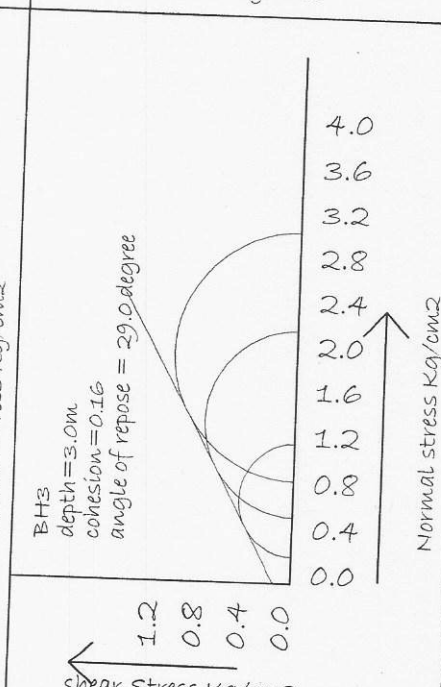
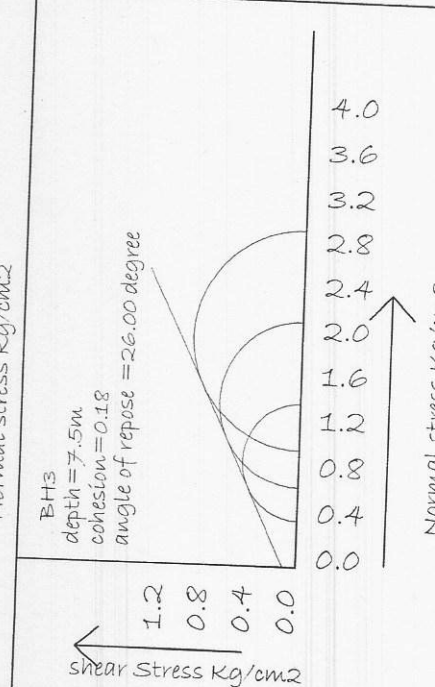
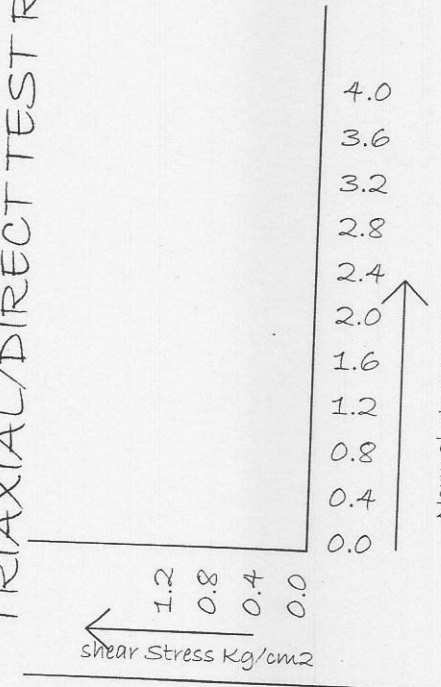
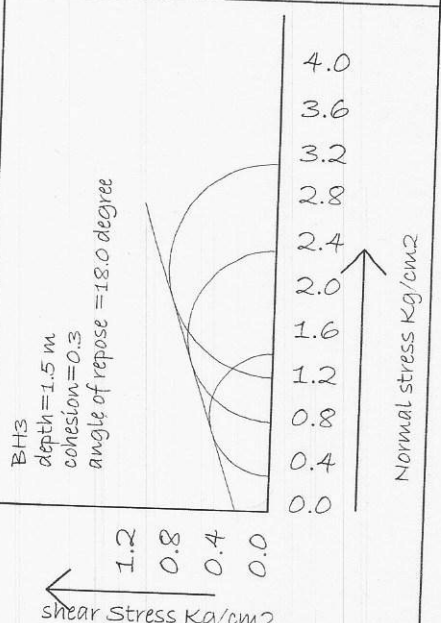
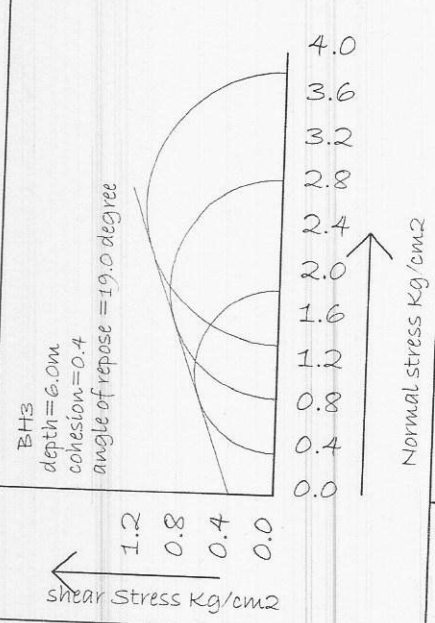
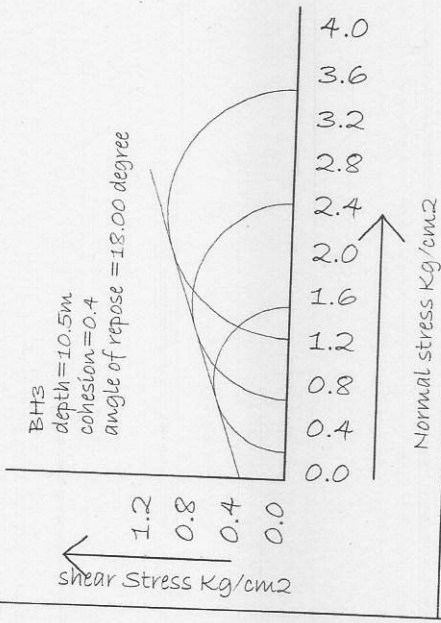
TRIAxIAL/DIRECT TEST RESULT



TRIAxIAL/DIRECT TEST RESULT

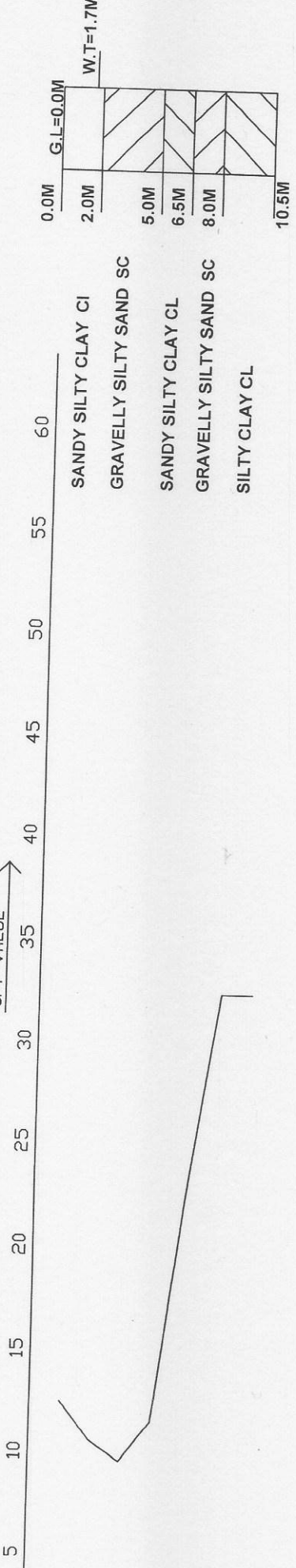


TRIAxIAL/DIRECT TEST RESULT



BORE LOG AND DEPTH ~ SPT GRAPH (C/O DEGREE COLLEGE AT ARWAL)

SPT VALUE →

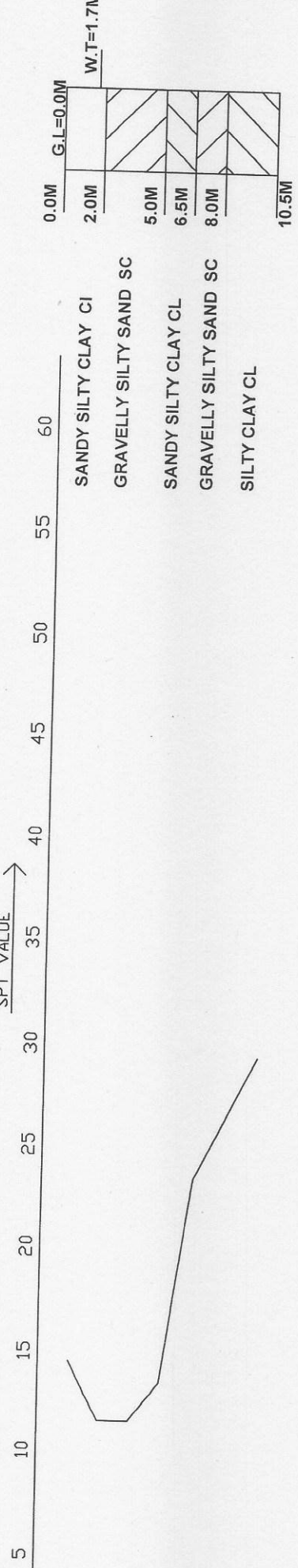


BORE LOG

BH1

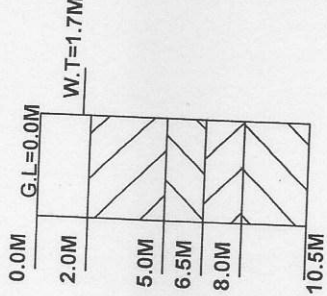
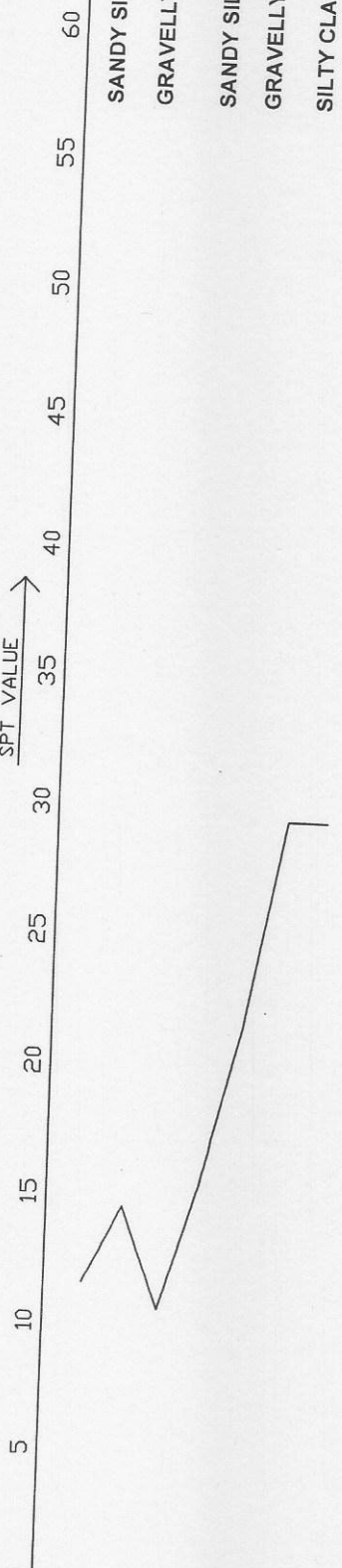
BORE LOG AND DEPTH ~ SPT GRAPH (C/O DEGREE COLLEGE AT ARWAL.)

SPT VALUE →



BORE LOG
BH2

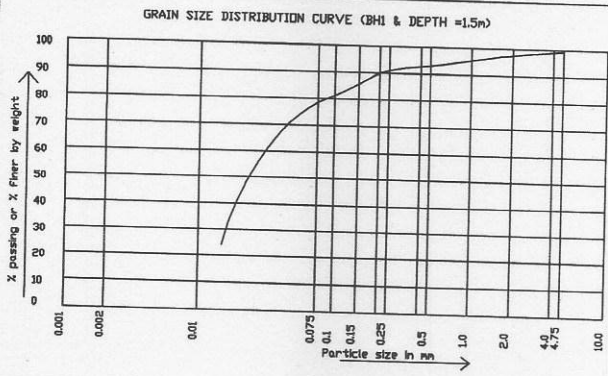
BORE LOG AND DEPTH ~ SPT GRAPH (C/D DEGREE COLLEGE AT ARWAL.)



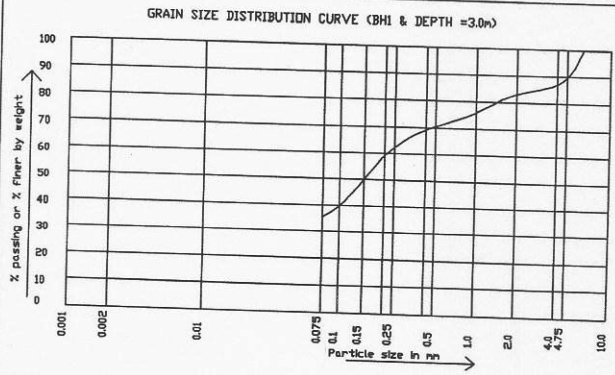
BORE LOG

BH3

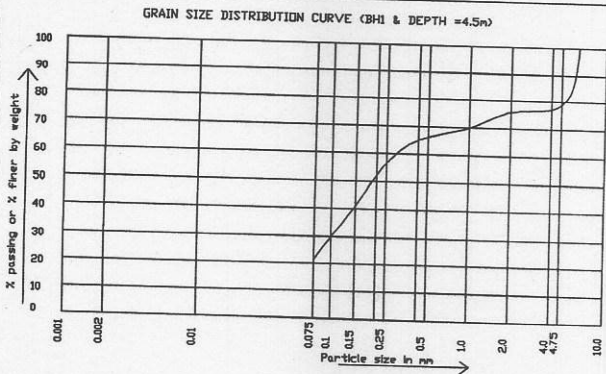
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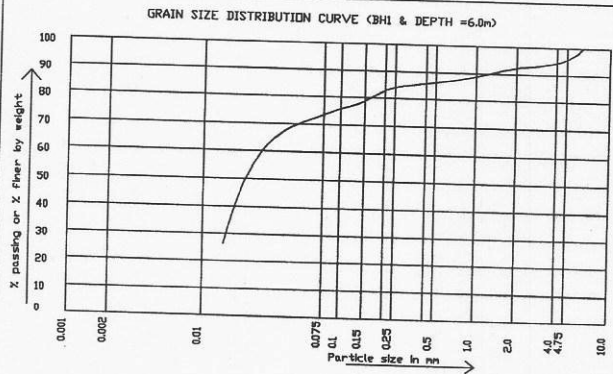
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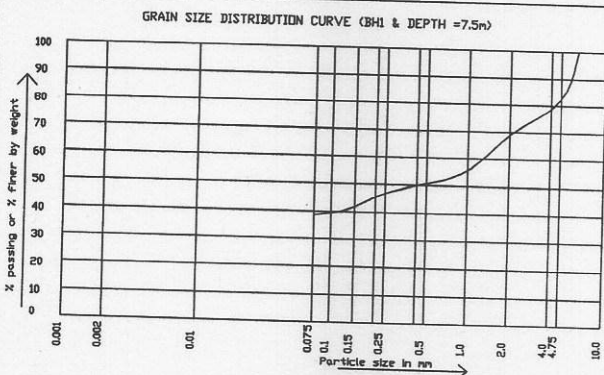
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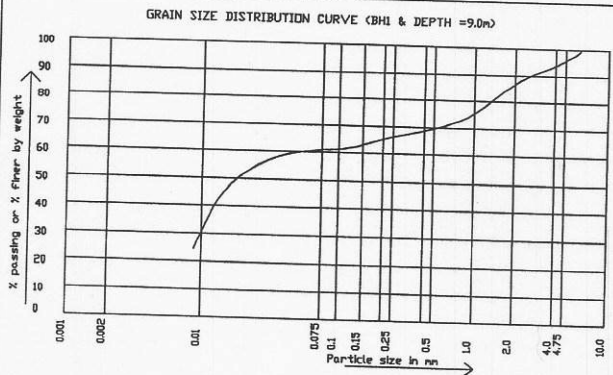
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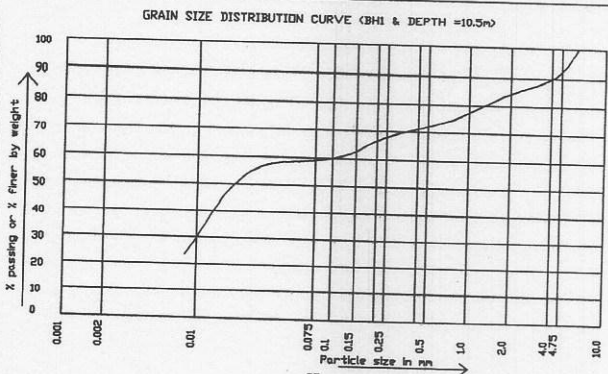
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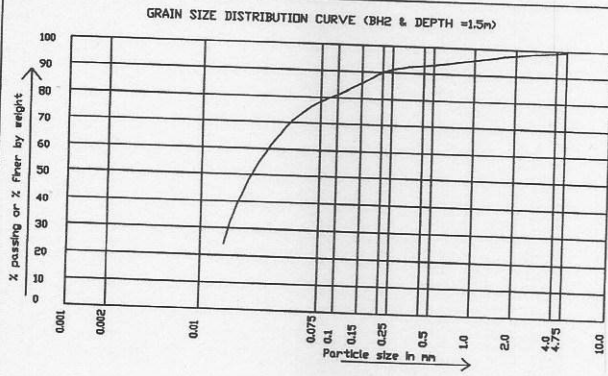
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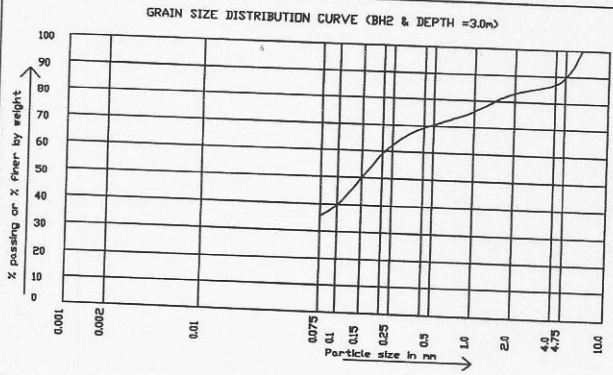
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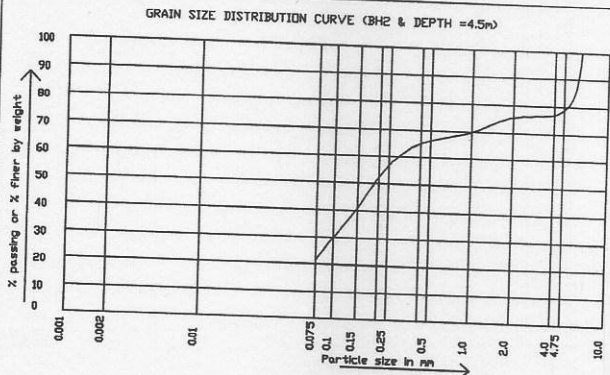
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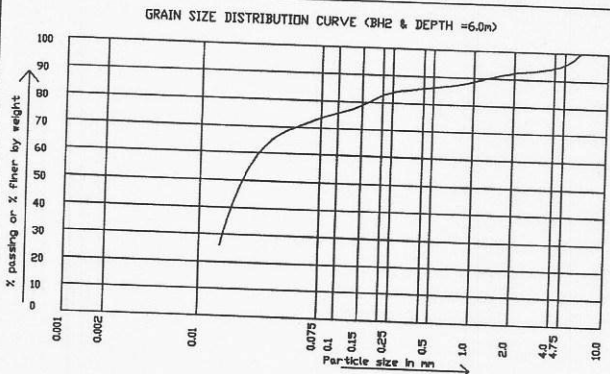
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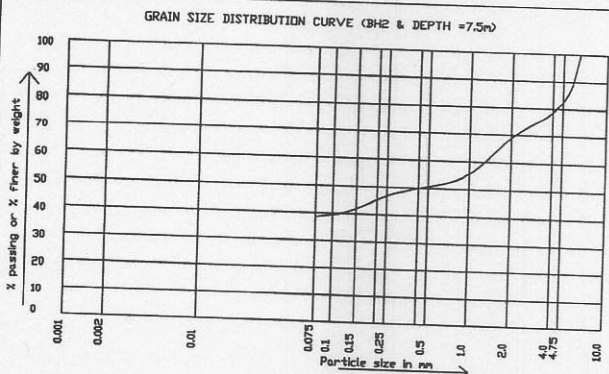
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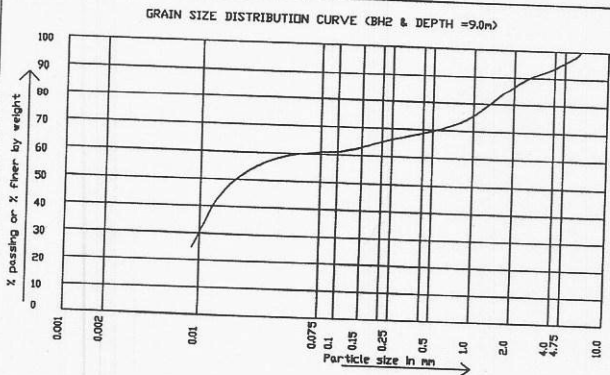
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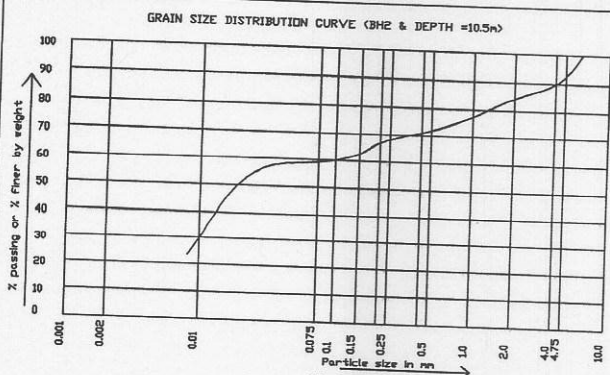
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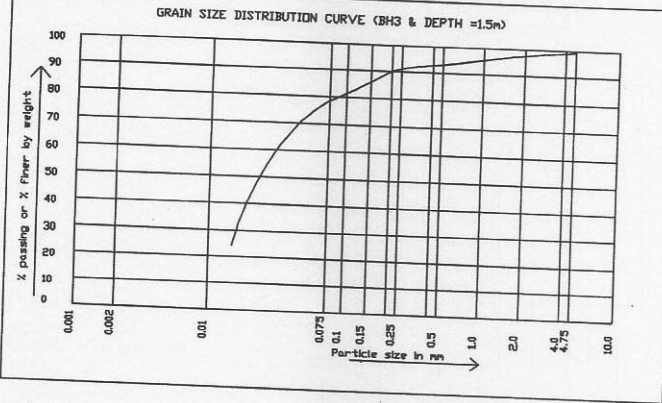
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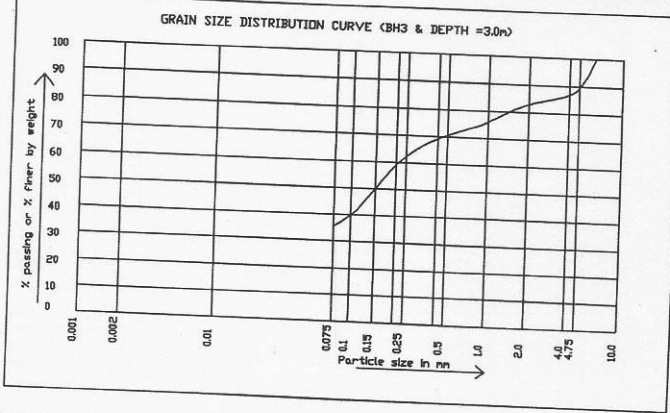
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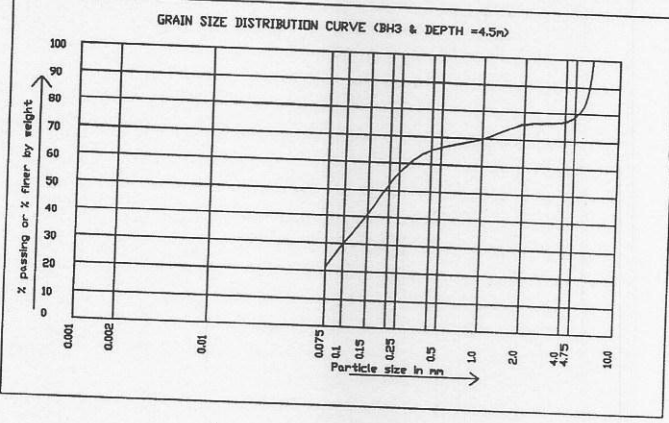
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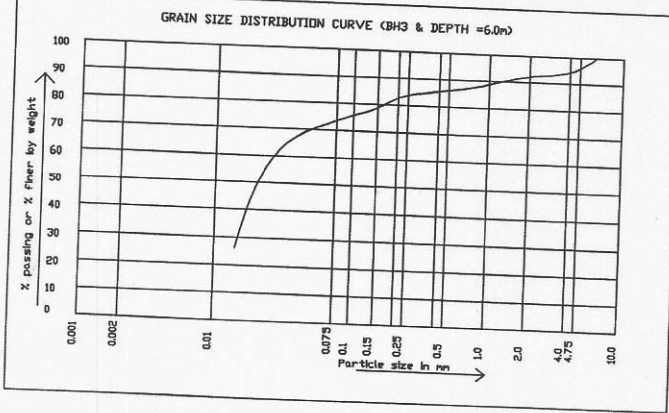
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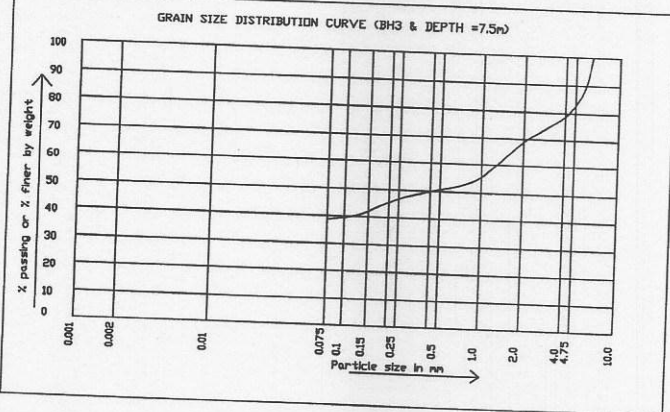
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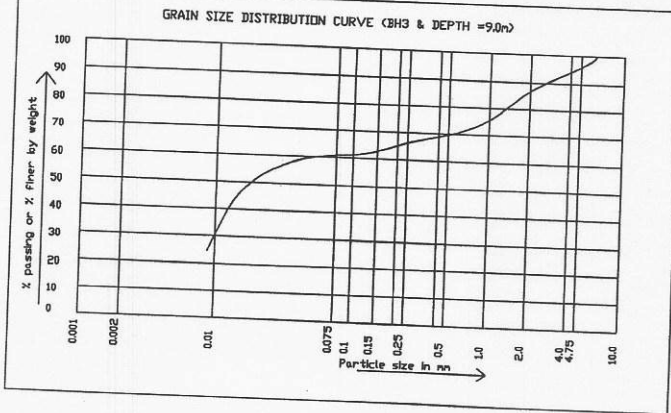
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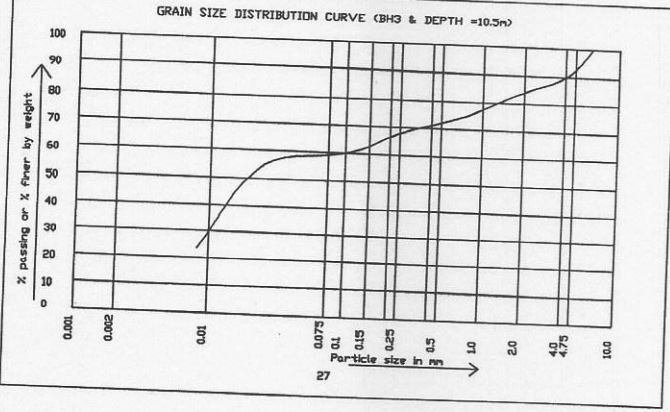
C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL



C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL



C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL



SOIL TEST FOR C/O DEGREE COLLEGE IN THE CAMPUS OF ARWAL DISTRICT HEADQUARTER, ARWAL

Calculation of Net safe Bearing Capacity for Strip Footing

Table 1 BEARING CAPACITY FACTORS AS PER IS 6403 : 1981

Angle of shearing resistance of soil, phi	Nc	Nq	Ny			
0	5.14	1	0			
5	6.49	1.57	0.45			
10	8.35	2.47	1.22			
15	10.98	3.94	2.65			
20	14.83	6.4	5.39			
25	20.72	10.66	10.88			
30	30.14	18.4	22.4			
35	46.12	33.3	48.03			
40	75.31	64.2	109.41			
45	138.88	134.88	271.76			
50	266.89	319.07	762.89			
Depth of footing below GL in meter, D=	1.5					
Width of footing in meter, B=	2					
Effective depth of soil formation contributing	2.8					
Average cohesion of soil mobilised in Ton/m ² =	2.20					
unit weight of soil in ton/m ² , y=	1.97					
Angle of shearing resistance of soil, phi, in degree =	22.77			Corresponding Nc/Nc= 11.53	Corresponding Nq/Nq= 4.29	Corresponding Ny/Ny= 3.04
Effective Angle of shearing resistance of soil, phi, in degree =	15.71			Corresponding Nc/Nc= 11.53	Corresponding Nq/Nq= 4.29	Corresponding Ny/Ny= 3.04
Depth factor, dc=	1.20	$dc=1+0.2*(D/B)*\tan(45+\phi/2)$				
Depth factor, dq=	1.10	$dq=1+0.1*(D/B)*\tan(45+\phi/2)$ if $\phi > 10$ otherwise $dq=1$				
Depth factor, dy=	1.10	$dy=1+0.1*(D/B)*\tan(45+\phi/2)$ if $\phi > 10$ otherwise $dy=1$				
effective surcharge at base level of foundation, q=yD	3.4	$q=yD$				
Q1 ton/m ² =	20.29	$Q1=(2/3)*c*Nc*dc$				
Q2 ton/m ² =	12.3046	$Q2=q*(Nq-1)*dq$				
Q3 ton/m ² =	1.62	$Q3=(1/2)*B*y*Ny*dy$ W				
ultimate bearing capacity Q ton/m ² =	34.2146	$Q=Q1+Q2+Q3$				
Factor of safety, F.S. =	3					
Net Safe Bearing Capacity in ton/m ² q=	11	$q=Q1/F.S.$				

Table 8

Soil stratification

DEPTH	SOIL TYPE	CONSISTANCY	CLASSIFICATION
0.0-2.0	SANDY SILTY CLAY	MEDIUM	CI
2.0-5.0	GRAVELLY SILTY SAND	MEDIUM	SC
5.0-6.5	SANDY SILTY CLAY	MEDIUM	CL
6.5-8.0	GRAVELLY SILTY SAND	MEDIUM	SC
8.0-10.5	SILTY CLAY	MEDIUM TO STIFF	CL

WATER TABLE was found at the depth of about 1.7m below GL as reported November'2019.

RECOMMENDATION

The present report is prepared on the basis of lab. Test result & field test conducted in the field. The lab. test result is obtained by conducting different test on representative sample obtained through 3 no. of bore holes whose location and depth were decided by the engineer-in-charge and shown in the bore hole location plan.

The laboratory test of soil samples obtained in all bore holes are given in Tables 2-7. Study of these tables reveals that the sub-soil strata :

- (a) Soil strata comprised of fine-grained soil & coarse grained soil in alternate layer till 10.5m depth.
- (b) Coarse grained soil consists gravel also.

Therefore, foundation should be placed at 1.50m or beyond the ground level. Both, shallow as well as deep, foundations are feasible. Pile bore may collapse due to presence of coarse grain soil. Therefore, Care should be taken to stabilize the bore hole. Presence of gravel & sand may cause trouble while making bore hole.

By way of example the calculated value of safe capacity of certain type and size of Shallow foundation are being tabulated below: -

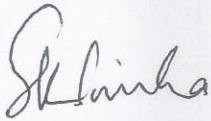
Strip foundation

Depth below GL (m)	Width of foundation (m)	Allowable bearing capacity(t/m ²)	Maximum expected settlement(mm)
1.5	2	10	60

Limitation

If the sub-soil condition is found much different from those reported here during trenching, suitable steps should be taken. Back filling over footing shall be done with proper compaction.

Pile capacity shall be confirmed by Initial and Routine pile load test as per relevant Indian codes.



SUBODH KUMAR SINHA
Partner Shamvvi Consultant